

Design and Assembly Analysis of Piston, Connecting Rod & Crankshaft

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Abstract:

The main function of the piston of an IC engine is to receive the impulse from the expanding gas and to transmit the energy to the crankshaft through the connecting rod. The piston must also disperse a large amount of heat from the combustion chamber to the cylinder walls. In this thesis is to Model & Assemble the Piston, Connecting Rod & Crankshaft for a 4-stroke air-cooled 150cc Engine by theoretical calculations & also to Compare the Structural Analysis & Modal Analysis on two different materials such as (Aluminum Alloy – Cast iron) for Piston, (Aluminum Alloy – Manganese steel) for Connecting Rod & (Nickel Chromium steel – High carbon steel) for Crankshaft. Modeling, Assembly of Piston, Connecting rod and Crankshaft is done in Creo/Engineering software & Analysis is done in ANSYS. Structural analysis is used to determine displacements & stresses under static. Modal Analysis is used to determine the Vibration characteristics (natural frequencies & mode shapes) of the three components. Thermal analysis is to determine the heat flux and temperature distribution. By comparing the displacement & stress results, using Cast Iron for Piston, Manganese Steel for Connecting rod and High Carbon Steel for crankshaft is best combination for assembly.

Keywords — Piston, Connecting rod and Crankshaft, Aluminum Alloy – Cast iron, Aluminum Alloy – Manganese steel, Nickel Chromium steel – High carbon steel, Creo/Engineering software, ANSYS.

I. INTRODUCTION

An internal combustion engine is defined as an engine in which the chemical energy of the fuel is released inside the engine and used directly for mechanical work, as opposed to an external combustion engine in which a separate combustor is used to burn the fuel. The internal combustion engine was conceived and developed in the late 1800s. It has had a significant impact on society, and is considered one of the most significant inventions of the last century.

A piston is a cylindrical plunger that moves within a metal cylinder through the four strokes of the engine cycle: intake, compression, power and exhaust. While their motion is predicated on other engine parts and the mixture of air and fuel, the motion of a piston is central to the functioning of an engine. In an engine, its purpose is to transfer force from expanding gas in the cylinder to the crankshaft via a piston and Connecting rod. In a pump, the function is reversed and force is transferred from the crankshaft to the piston for the purpose of compressing or ejecting the fluid in the cylinder. In a reciprocating piston engine, connecting rod

connects the piston to the crank or crankshaft. In modern automotive internal, the connecting rods are most usually made of steel for production engines, but can be made of aluminum (for lightness and the ability to absorb high impact at the expense of durability) or titanium (for a combination of strength and lightness at the expense of affordability) for high performance engines, or of cast iron for applications such as motor scooters. They are not rigidly fixed at either end, so that the angle between the connecting rod and the piston can change as the rod moves up and down and rotates around the crankshaft. Condors', especially in racing engines, may be called "billet" rods, if they are machined out of a solid billet of metal, rather than being cast. The connecting rod is the intermediate member between the piston and the Connecting Rod. Its primary function the push and pull from the piston pin to the crank pin and thus converts the reciprocating motion of the piston into rotary motion of the crank. The connecting rod is under tremendous stress from the reciprocating load represented by the piston, actually stretching and being compressed with every rotation, and the load increases to the third

power with increasing engine speed.

The crankshaft, sometimes casually abbreviated to crank, is the part of an engine which translates reciprocating linear piston motion into rotation. To convert the reciprocating motion into rotation, the crankshaft has "crank throws" or "crankpins", additional bearing surfaces whose axis is offset from that of the crank, to which the "big ends" of the connecting rods from each cylinder attach.

Crankshafts can also be machined out of a billet, often using a bar of high quality vacuum remelted steel. Even though the fiber flow (local in homogeneities of the material's chemical composition generated during casting) doesn't follow the shape of the crankshaft (which is undesirable), this is usually not a problem since higher quality steels which normally are difficult to forge can be used. These crankshafts tend to be very expensive due to the large amount of material removal which needs to be done by using lathes and milling machines, the high material cost and the additional heat treatment required. However, since no expensive tooling is required, this production method allows small production runs of crankshafts to be made without high costs.

II. LITERATURE SURVEY

In this study, the modal analysis results are verified by a modal testing experiment. C. Azoury et al [1] presented a report on the experimental and analytical modal analysis of a crankshaft. The effective material and geometrical properties are measured, and the dynamic behavior is investigated through impact testing. The three dimensional finite element models are constructed and an analytical modal analysis is then performed to generate natural frequencies and mode shapes in the three-orthogonal directions. The finite element model agrees well with the experimental tests and can serve as a baseline model of the crankshaft. R. J. Deshbhratar, et al [2] analyzed 4- cylinder crankshaft and model of the crankshaft were created by using Pro/E Software and then imported to ANSYS software. The maximum deformation appears at the centre of crankshaft surface. The maximum stress appears at the fillets between the crankshaft journal and crank cheeks, and near the central point. The edge of

main journal is high stress area. The crankshaft deformation was mainly bending deformation under the lower frequency. And the maximum deformation was located at the link between main bearing journal and crankpin and crank cheeks. So this area prone to appear the bending fatigue crack. Abhishek choubey, and et al [3] have analyzed crankshaft model and 3-dimensional model of the crankshaft were created by SOLID WORKS Software and imported to ANSYS software. The crankshaft maximum deformation appears at the centre of crankpin neck surface. The maximum stress appears at the fillets between the crankshaft journals and crank cheeks and near the central point journal. The edge of main journal is high stress area. Rinkle garg et al. [4] Analyzed crankshaft model and crank throw were created by using Pro/E Software and then imported to ANSYS software. The result shows that the improvement in the strength of the crankshaft as the maximum limits of stress, total deformation, and the strain is reduced. The weight of the crankshaft is reduced. There by, reduces the inertia force. As the weight of the crankshaft is decreased this will decrease the cost of the crankshaft and increase the I.C engine performance. Sanjay B Chikalthankar et al [5] investigated stresses developed in crankshaft under dynamic loading. In this study a dynamic simulation was conducted on crankshaft, Finite element analysis was performed to obtain the variation of stress magnitude at critical locations. This load was then applied to the FE model, and boundary conditions were applied according to the engine mounting conditions. The analysis was done for different engine speeds and as a result critical engine speed and critical region on the crankshaft were obtained. Stress variation over the engine cycle and the effect of torsional load in the analysis were investigated. Results obtained from the analysis are very useful in optimization of the crankshaft.

III. OBJECTIVE AND SCOPE OF THE WORK

The objectives of this project is to design and analysis of Piston, connecting rod and crank shaft assembly by using CREO design software and Ansys for requirement of better engine performance with different alloy materials.

The following scopes of the project are determined in order to achieve the objectives of the project:

Design the flexible raw materials for automobile components.

Analysing best strength of the raw materials

IV. CALCULATIONS

Design calculations of piston

Density of diesel = 820 to 950 kg/cm at 15°c

= 0.00095 kg/cm³

Density = 0.00000095 kg/mm³

Diesel C₁₀H₂₂ to C₁₅H₂₈ = C₁₅ H₂₈

Molecular weight of C₁₅H₂₈ = 208g/mole

Mass = density × volume

m = 0.00000095 × 130000

m = 1.235

R = 8.3143 J/mol K

$$P = \frac{mrt}{v} = \frac{1.235 \times 8.3143 \times 288}{0.208 \times 0.001300}$$

= 10936107.69 J/m³

P = 10.936 N/mm²

Piston Head

Gas pressure p = 10.936 N/mm²

Outside diameter of piston = 72.5

σ_t = bending tensile stress = 35-40Mpa

Temperature at the centre of the piston head T_c = 425°c to 450°c

Temperature at the edge of the piston head T_e = 200°c to 225°c

$$T_c - T_e = 220^\circ c \quad t_h = \sqrt{\frac{(3P \times D^2)}{16\sigma t}}$$

$$= \sqrt{\frac{(3 \times 10.936 \times 72.5^2)}{16 \times 40}}$$

$$= 16.41 \text{ mm}$$

Thickness of the ribs = t_h / 2 = t_h / 3
= 5.47 (or) 8.20 mm

Piston Rings

Radial thickness of the ring

$$t_1 = D \times \sqrt{\frac{3p_w}{\sigma t}}$$

P_w = pressure of gas on the cylinder wall

P_w = 0.025 to 0.042 N/mm²

σ_t = 85 Mpa to 110 Mpa for CI rings

$$t_1 = 72.5 \times \sqrt{\frac{3 \times 0.042}{110}} = 2.45 \text{ mm.}$$

Axial thickness t₂ = D/10n_R

n_R = no. of rings = 3

$$t_2 = \frac{72.5}{10 \times 3} = 2.41 \text{ mm.}$$

Width of top land b₁ = t_h to 1.2 t_h = 16.41 to 19.692 mm

The width of other ring land (distance between the ring grooves)

b₂ = 0.75t₂ to t₂ = 1.8075 to 2.41 mm

The gap between the free ends of the ring =

3.5t₁ to 4t₁

= 8.575 to 9.8 mm

Piston Barrel (Cylindrical portion of the Piston)

Thickness of piston barrel

t₃ = radial depth of piston ring groove

b = t₁ + 0.4 = 2.85mm

t₃ = 0.03 × 69.6 + 2.75 + 4.5 = 9.525mm

The piston wall thickness towards the open end

t₄ = 0.25t₃ to 0.35t₃

t₄ = 3.33mm

Piston Skirt

Maximum gas load on the piston

$$P = P \times \frac{\pi}{4} D^2$$

P = maximum gas pressure

$$P = 10.936 \times \frac{\pi}{4} 72.5^2$$

P = 45226.79866 N

Maximum side thrust on the cylinder

$$R = \frac{P}{10} = 4522.67 \text{ N}$$

Length of the piston skirt

L = 0.65D to 0.8D = 58 mm

Length of ring section = 7 × b₂ = 16.87

Total length of the piston

L = length of the skirt + length of the ring section

+ top land

= 58 + 16.84 + 19.692

= 94.532 mm.

Piston pin (gudgeon pin or wrist pin)

d_o = outside diameter of the piston pin

l₁ = length of the piston pin in the bush of the

small end of the connecting rod

= 0.45D = 0.45 × 69.6

l₁ = 32.625 mm

Load on the piston due to gas pressure

p = 45226.79866 N

Load on the piston pin due to bearing pressure or

bearing load = bearing pressure × bearing area

P = p_{b1} × d_o × l₁

p_{b1} = bearing pressure at the small end of the

connecting rod bushing

$$d_o = \frac{P}{p_{b1} \times l_1}$$

Bearing pressure of tin bronze = 50Mpa

$$d_o = \frac{45226.7986}{50 \times 32.625}$$

d_i = 0.6d_o = 16.635mm

Length between the supports

$$l_2 = \frac{l_1 + D}{2} = \frac{32.625 + 72.5}{2}$$

$$l_2 = 52.56\text{mm}$$

The mean diameter of the piston bosses = 1.4 d_o
= 38.815mm

Design calculations of connecting rod

Dimensions of cross section of connecting rod

Thickness of flange & web of the section = t

Width of section $B = 4t$

Height of section $H = 5t$

Area of section $A = 2(4t \times t) + 3t \times t$

$$A = 11t^2$$

MI of section about x axis

$$I_{xx} = \frac{1}{12} (4t(5t)^3 - 3t(3t)^3) = 419 \times 12t^4$$

MI of section about y axis

$$I_{yy} = (2 \times \frac{1}{12} t(4t)^3 + \frac{1}{12} (3t)t^3) = 131 \times 12t^4$$

$$I_{xx} \setminus I_{yy} = 3.2$$

Length of connecting rod = 2 times the stroke

$$L = 2 \times 80.5 = 161\text{mm}$$

Buckling load $W_B = \text{maximum gas force} \times \text{F.O.S}$

$$W_B = 70924.49978 \times 6 = 425546.9987$$

$$W_B = \frac{\sigma_c \times A}{1 + a(L \setminus K_{xx})^2}$$

σ_c = compressive yield stress = 386 Mpa

$$K_{xx} = I_{xx} \setminus A \frac{419 \times 12t^4}{11t^2}$$

$$= 3.17t^2$$

$$k_{xx} = 1.78t$$

f_c = maximum load

$$f_c = p = 70924.49978$$

$$a = f_c \setminus \pi^2 E$$

$$a = 70924.49978 \setminus \pi^2 68900$$

$$a = 0.1044$$

$$425546.9987 = \frac{386 \times 11t^2}{1 + 0.1044(161 \setminus 1.78t)^2}$$

$$11t^4 - 1102.4533t^2 - 820135.3636 = 0$$

$$t^2 = \frac{100.22 \pm \sqrt{((100.22)^2 + 4 \times 820135.3636)}}{2}$$

$$t^2 = \frac{100.22 \pm 1813.9983}{2}$$

$$t = 30.93$$

Width of section $B = 4t = 123.74\text{mm}$

Height of section $H = 5t = 154.65\text{mm}$

$$\text{Area } A = 11t^2 = 10523.3139\text{mm}^2$$

Height at the big end (crank end) = $H_2 = 1.1H$ to $1.25H$

$$H_2 = 170.115\text{mm}$$

Height at the small end (piston end) = $0.9H$

$$H_1 = 139.185\text{mm}$$

Dimensions of crank pin

Load on the crank pin = projected area \times bearing pressure

$$F_L = d_c \times l_c \times p_{bc}$$

$$l_c = 1.25 d_c \text{ to } 1.5d_c$$

$$F_L = 1.5 d_c^2 \times p_{bc}$$

p_{bc} = allowable bearing pressure at the crank pin bearing

$$p_{bc} = 12.5\text{N/mm}^2$$

$$F_L = \frac{\pi D^2}{4} \times p = 70924.49978$$

$$70924.49978 = 1.5 d_c^2 \times 12.5$$

$$d_c^2 = 2750.7708$$

$$d_c = 61.503$$

$$l_c = 1.5d_c = 78.66$$

Design of crankshaft

Specifications

Tata Indica vista 1.3 diesel engine specifications

Bore diameter or cylinder bore = $D = 69.6\text{mm}$

Stroke = 82mm

Explosion pressure gas pressure = $P = 15.454\text{N/mm}^2$

Maximum torque = 200 N-m @ 1750-3000 rpm

Design of crank shaft when the crank is at the dead centre

We know that piston gas load

$$F_p = \frac{\pi}{4} \times D^2 \times P = \frac{\pi}{4} \times 69.6^2 \times 15.454 =$$

$$41585.951\text{N}$$

Now the various parts of the crank shaft are design as discussed below:

Design of Crank Pin for Crank shaft

Let d_c = diameter of crank pin mm

l_c = length of the crank pin = $0.8 d_c$ considering

the crank pin in bearing taking $p_b = 15\text{N/mm}^2$

We have = $F_p = d_c \times l_c \times p_b = 41585.951 = d_c$

$$\times 0.8d_c \times 15 = 8d_c^2$$

$$d_c = 72\text{mm}$$

$$l_c = 0.8d_c = 58\text{mm}$$

Let us now the included bending stress in the crank pin

We know that bending moment at the crank pin

$$M = \frac{3}{4} F_p \times l_c = \frac{3}{4} \times 41585.951 \times 58 =$$

$$1808988.869\text{N/mm}$$

Section modulus of the crank pin $Z = \frac{\pi}{32} d_c^3 =$

$$\frac{\pi}{32} \times 72^3 = 36624.96\text{mm}^3$$

$$\text{Bending stress induced } \frac{M}{Z} = \frac{1808988.869}{36624.96} =$$

$$49.39\text{N/mm}^2$$

The induced bending stress is within in the permissible limits of 560 Mpa, therefore design of crank pin is safe

Design of bearings for Crank shaft

Let d_1 = diameter of the bearing

Let us take thickness of the crank web

$$t = 0.6d_c = 0.6 \times 72 = 43\text{mm}$$

Length of bearing $l_1 = 1.7d_c = 1.7 \times 72 = 122.4\text{mm}$

WKT bending moment at centre of bearing

$$M = F_p(0.75l_c+t+0.5l_1) = 41585.951(0.75 \times 58+43+0.5 \times 122) = 6133927.773$$

Bending moment (M) WKT

$$6133927.773 = \frac{\pi}{32} d_1^3 \sigma_b = \frac{\pi}{32} d_1^3 \times 560 = 54.95$$

$$d_1^3$$

$$d_1 = 48\text{mm}$$

Design of crank web for Crank shaft

Let w = width of the crank web in mm

WKT bending moment on the crank web

$$M = F_p(0.75l_c+t+0.5l_1) = 41585.951(0.75 \times 58+43+0.5 \times 43) = 2703086.815$$

$$\text{Section modulus } Z = \frac{1}{6} \times w \times t^2 = \frac{1}{6} \times w \times 43^2 =$$

$$308.166wt$$

$$\text{Bending stress } \sigma_b = \frac{M}{Z} = \frac{41585.951}{w \times 43} = \frac{967.115}{w}$$

Total stress on the crank web $\sigma_t = \sigma_b + \sigma_d =$

$$\frac{967.115}{w} + \frac{8771.509}{w} = \frac{9738.625}{w}$$

Total stress should not exceed permissible limit of 560 Mpa

$$560 = \frac{9738.625}{w}$$

$$W = 17.390 = 20\text{mm}$$

V. MATERIALS AND PROPERTIES

Cast Iron, Aluminum Alloy and Cast Steel etc. are the common materials used for piston of an Internal Combustion Engine. Cast Iron pistons are not suitable for high speed engines due its more weight. These pistons have greater strength and resistance to wear. The Aluminum Alloy Piston is lighter in weight and enables much lower running temperatures due to its higher thermal conductivity. The coefficient of expansion of this type of piston is about 20% less than that of pure aluminum piston but higher than that of cast iron piston and cylinder wall. To avoid seizure because of higher expansion than cylinder wall, more piston clearance required to be provided.

Connecting rods are made with balancing bosses so that their weight can be adjusted to specifications.

Steel is normally used for construction of automobile connecting rods because of its strength, durability, and lower cost. However, steel with its high mass density exerts excessive stresses on the crankshaft of a high speed engine. This in turn requires a heavier crankshaft for carrying the loads and, therefore, the maximum RPM of the engine is limited. Additionally, higher inertia loads, such as those

caused by steel connecting rods and heavier crankshafts reduces the acceleration or deceleration rates of engine speed. Therefore, light alloy metals such as aluminum and titanium are currently being used in high speed engine connecting rods to circumvent the above-mentioned problems. Titanium has better mechanical properties than aluminum, at the expense of higher density and cost. This higher density and cost have made aluminum connecting rods more popular and attractive. However, they suffer from relatively low strength and fatigue life.

Crankshaft is usually made by steel. Generally medium –carbon steels alloys are composed of iron small percentage of carbon (0.25% to 0.45%), along with combinations of several alloying elements, the mix of which. The alloying elements typically used in these carbon steels are manganese, chromium, molybdenum, nickel, silicon, cobalt, vanadium, and sometimes aluminium and titanium. In addition to alloying elements, high strength steels are carefully refined so as to remove as many of the undesirable impurities as possible like sulphur phosphorous, calcium, etc. the highest quality steels are also used. The required purity can often only be achieved by melting in a vacuum, then re-melting in a vacuum to further refine the metal. Typical vacuum processing methods are VIM and VAR.

Used materials for piston

Aluminum 360, aluminum alloy 6061, cast iron

Used materials for connecting rod

Aluminum 360, aluminum alloy 6061 and manganese steel.

Used materials for crankshaft

Nickel chromium and high carbon steel.

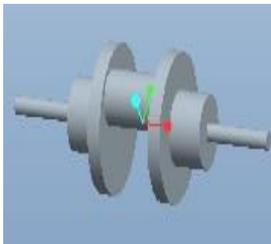
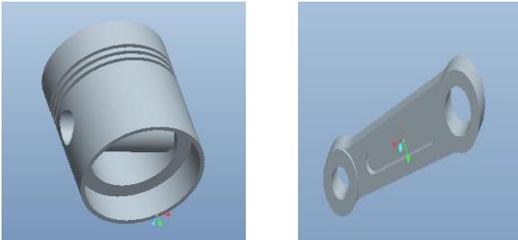
Properties of different alloy materials for piston, connecting rod and crank shaft

Table: 1 Properties of different alloy materials for piston, connecting rod and crank shaft

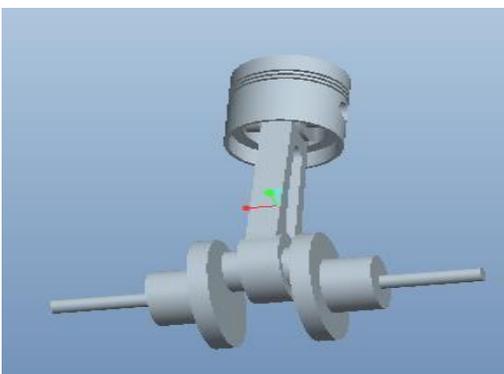
| S.NO | NAME OF THE MATERIAL | DENSITY | YOUNGS MODULUS | POISSON'S RATIO | THERMAL CONDUCTIVITY |
|------|----------------------|----------|----------------|-----------------|----------------------|
| 1 | ALUMINUM ALLOY 6061 | 2.70g/CC | 68.9Gpa | 0.33 | 180w/m-k |
| 2 | ALUMINUM ALLOY 360 | 2.68g/CC | 71.0Gpa | 0.33 | 113w/m-k |
| 3 | CAST IRON | 7.81g/CC | 240Gpa | 0.24 | 113w/m-k |
| 4 | NICKEL CHROMIUM | 8.42g/CC | 207Gpa | 0.36 | 30w/m-k |
| 5 | MANGANESE STEEL | 8.0g/CC | 210Gpa | 0.29 | 50w/m-k |
| 6 | HIGH CARBON STEEL | 7.8g/CC | 200Gpa | 0.295 | 52.0w/m-k |

VI. MODELING

PTC CREO, formerly known as Pro/ENGINEER, is 3D modeling software used in mechanical engineering, design, manufacturing, and in CAD drafting service firms. It was one of the first 3D CAD modeling applications that used a rule-based parametric system. Using parameters, dimensions and features to capture the behavior of the product, it can optimize the development product as well as the design itself. PTC Creo says it can offer a more efficient design experience than other modeling software because of its unique features including the integration of parametric and direct modeling in one platform. By using Creo software, I did modeling of piston, connecting rod and crankshaft. I assembled these all together in Creo software.



Modeling Parts of piston, connecting rod and crank shaft in 3D view

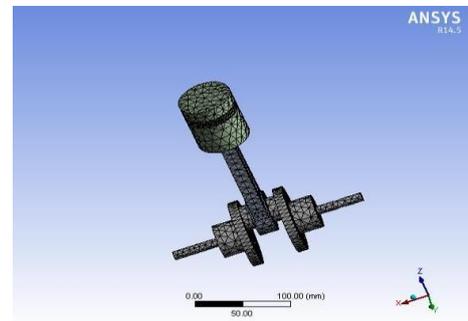


Assembly of piston, connecting rod and crank shaft in 3D view

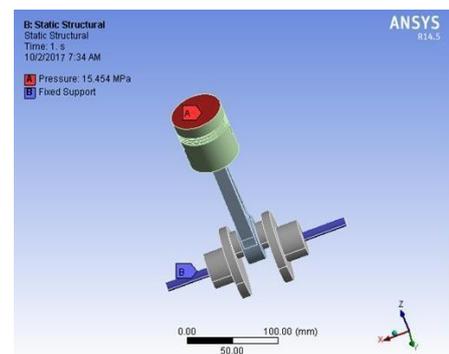
VII. ANALYSIS TOOL(ANSYS)

The software uses the finite element method (FEM). FEM is a numerical technique for analyzing Engineering designs. FEM divides the model into many small pieces of simple shapes called elements effectively replacing a complex problem by many simple problems that need to be solved simultaneously. I did structural analysis, thermal analysis and model analysis with using ANSYS software. FEM is accepted as the standard analysis method due to generality and suitability for computer implementation.

MESHED MODEL

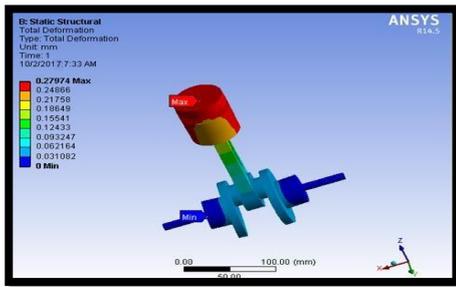


BOUNDARY CONDITIONS

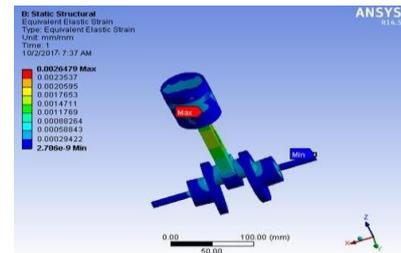


STATIC ANALYSIS

Materials for Piston and Connecting Rod Aluminum Alloy 360 and Crank Shaft Nickel Chromium

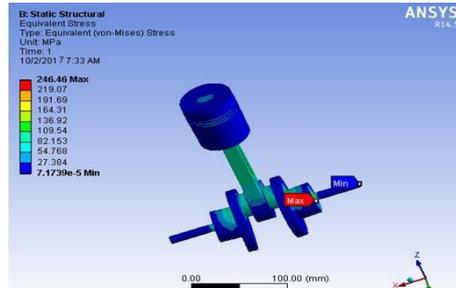


Total Deformation

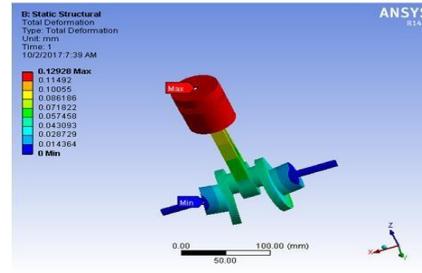


Equivalent strain

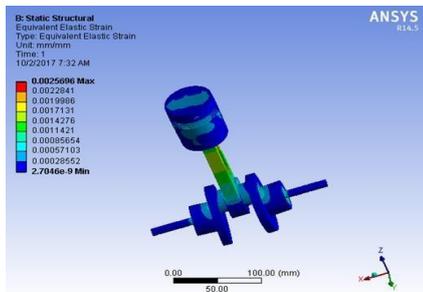
Materials for piston-cast iron and connecting Rod manganese for crankshaft high carbon Steel



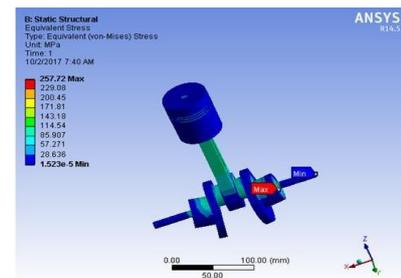
Equivalent stress



Total Deformation

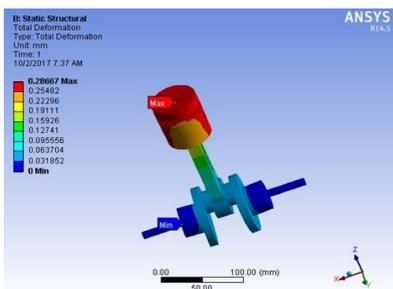


Equivalent strain

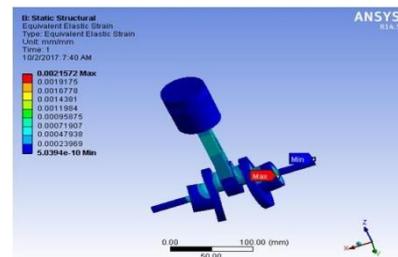


Equivalent stress

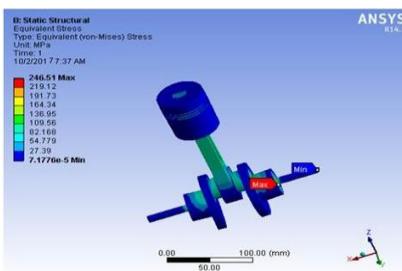
Materials for Piston and Connecting Rod Aluminum Alloy6061 and Crank Shaft Nickel Chromium



Total Deformation



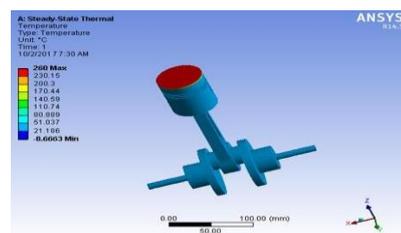
Equivalent strain



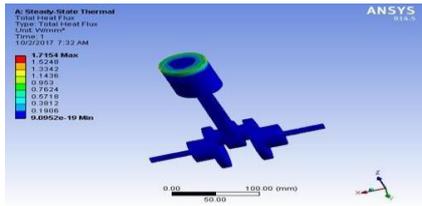
Equivalent stress

THERMAL ANALYSIS

Materials for piston and connecting rod aluminum alloy 360 for crank shaft nickel chromium

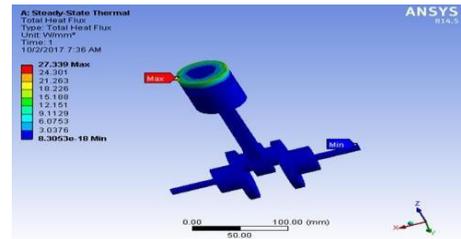


Temperature Distribution

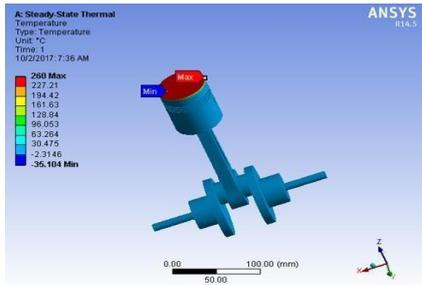


Heat flux

Materials for piston and connecting rod aluminum alloy 6061 for crank shaft nickel chromium



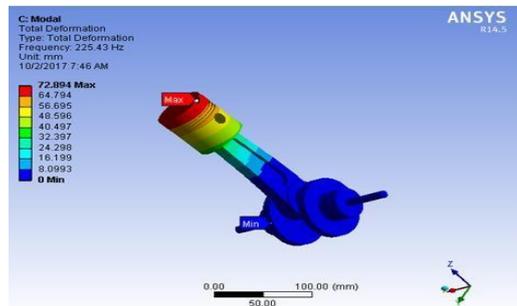
Heat flux



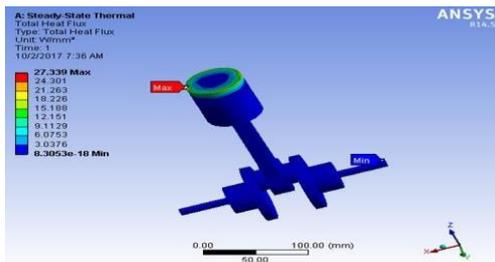
Temperature Distribution

MODAL ANALYSIS

Materials for piston and connecting rod aluminum alloy 360 for crank shaft nickel chromium

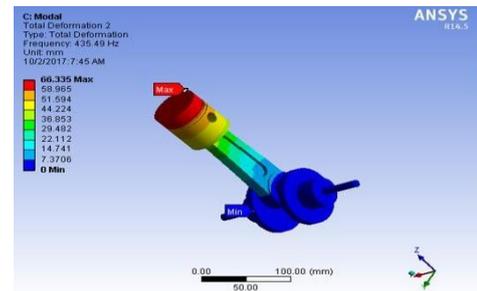


Total Deformation-1

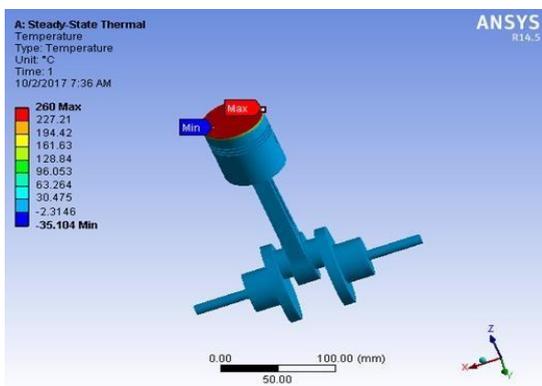


Heat flux

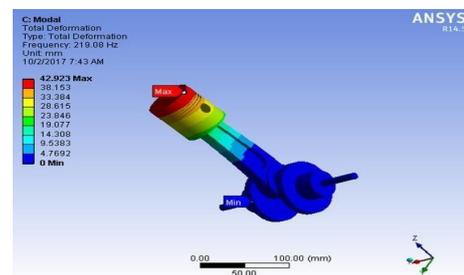
Materials for piston – cast iron and connecting rod manganese steel for crank shaft high carbon steel



Total Deformation-2

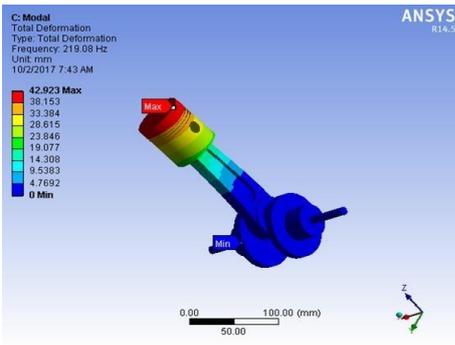


Temperature distribution

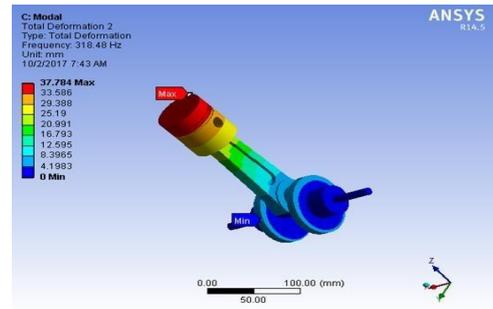


Total Deformation-3

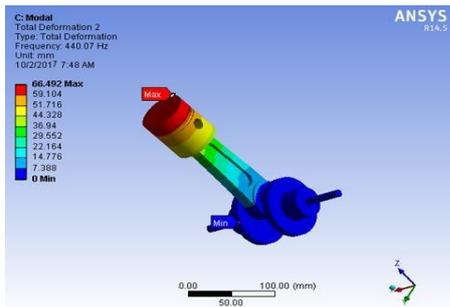
Materials for piston and connecting rod aluminum alloy6061 for crank shaft nickel chromium



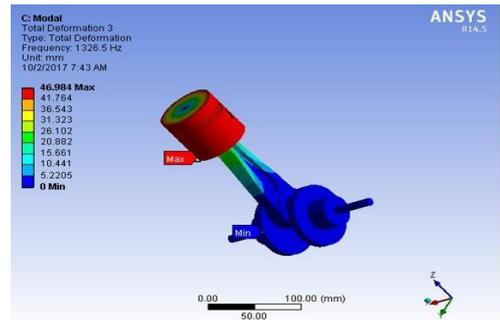
Total Deformation-1



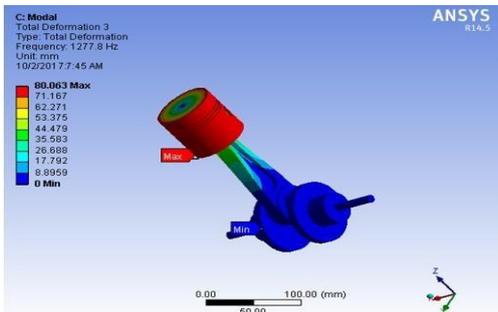
Total Deformation-2



Total Deformation-2

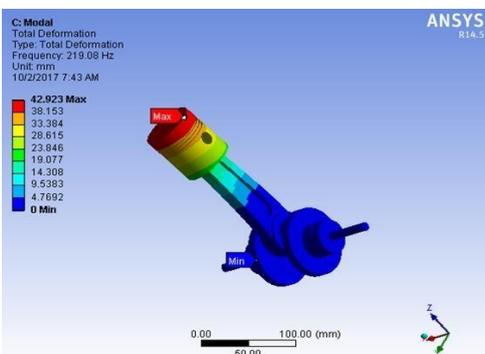


Total Deformation-3



Total deformation-3

Materials for piston – cast iron and connecting rod manganese steel for crank shaft high carbon steel



Total Deformation-1

VIII. RESULTS

a) STATIC ANALYSIS RESULTS

Table: 2 Static analysis results

| material | Deformation(mm) | Stress(MPa) | strain |
|--|-----------------|-------------|-----------|
| Materials for piston and connecting rod aluminum alloy 360 For crank shaft nickel chromium | 0.27974 | 246.46 | 0.0025696 |
| Materials for piston and connecting rod aluminum alloy6061 For crank shaft nickel chromium | 0.28667 | 246.51 | 0.0026479 |
| Materials for piston – cast iron and connecting rod manganese steel For crank shaft high carbon steel | 0.12928 | 257.72 | 0.0021572 |

b) THERMAL ANALYSIS RESULTS

Table: 3 Thermal analysis results

| material | Temperature(^o C) | Heat flux(w/mm ²) |
|---|------------------------------|-------------------------------|
| Materials for piston and connecting rod aluminum alloy 360 For crank shaft nickel chromium | 260 | 1.7154 |
| Materials for piston and connecting rod aluminum alloy6061 For crank shaft nickel chromium | 260 | 27.339 |
| Materials for piston – cast iron and connecting rod manganese steel For crank shaft high carbon steel | 260 | 8.0922 |

c) MODEL ANALYSIS RESULTS

Table: 4 Modal analysis results

| Mode shapes | Results | Materials for piston and connecting rod aluminum alloy 360 For crank shaft nickel chromium | Materials for piston and connecting rod aluminum alloy6061 For crank shaft nickel chromium | Materials for piston – cast iron and connecting rod manganese steel For crank shaft high carbon steel |
|-------------|------------------|---|---|--|
| Mode1 | Deformation (mm) | 73.191 | 72.894 | 42.923 |
| | Frequency(Hz) | 229.36 | 225.43 | 219.08 |
| Mode2 | Deformation (mm) | 66.492 | 66.335 | 37.784 |
| | Frequency(Hz) | 440.07 | 435.49 | 318.48 |
| Mode3 | Deformation (mm) | 80.36 | 80.063 | 46.984 |
| | Frequency(Hz) | 1302.18 | 1277.8 | 1326.5 |

CONCLUSION

- In this thesis is to Model & Assemble the Piston, Connecting Rod & Crankshaft for a 4-stroke air-cooled 150cc Engine by theoretical calculations & also to Compare the Structural Analysis & Modal Analysis on two different materials such as (Aluminum Alloy – Cast iron) for Piston, (Aluminum Alloy – Manganese steel) for Connecting Rod & (Nickel Chromium steel – High carbon steel) for Crankshaft.
- By observing the analysis results, the stress values are less than the respective yield stress values for

both the materials. The stress values are less for Aluminum alloy 360.

- By observing the modal analysis, the deformation values are more for aluminum alloy 360 at mode 3.
- Thermal analysis, the heat transfer rate is more for aluminum alloy6061.
- So it can be concluded that using Aluminum alloy 360 for piston and connecting rod is better considering weight and analysis results.

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